

PATENT ABSTRACTS OF JAPAN

(11)Publication number : 09-245802

(43)Date of publication of application : 19.09.1997

(51)Int.Cl. H01M 4/86
H01M 8/02
H01M 8/10

(21)Application number : 08-082106 (71)Applicant : TANAKA KIKINZOKU KOGYO

KK
WATANABE MASAHIRO
STONEHARD ASSOC INC

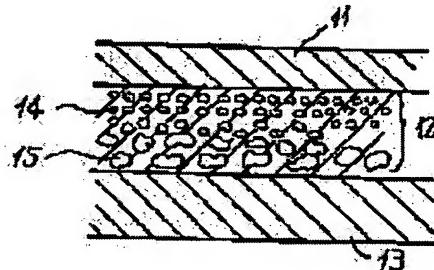
(22)Date of filing : 11.03.1996 (72)Inventor : TADA TOMOYUKI
TOSHIMA YASUHITO
TADANO ETSUKO

(54) ELECTRODE FOR POLYMER SOLID ELECTROLYTE TYPE FUEL CELL

(57)Abstract:

PROBLEM TO BE SOLVED: To improve gas permeability and conductivity of protons and electrons by making the performance of a catalyst layer differing in the thickness direction.

SOLUTION: In the case the preciseness of a catalyst carrier, as the performance of a catalyst layer, is made different in the direction of the thickness of the catalyst layer, the following function is provided. An ion exchange membrane 11 side of the catalyst layer 12 is made of a precise carrier 14 and a gas diffusion layer 13 side is made of a porous carrier 15. A fuel gas, e.g. hydrogen and oxygen, is supplied from the lower side of the gas diffusion layer 13 and since the layer is porous, the gas can easily pass through the layer and reaches the interface of both catalyst carriers 14, 15. Since the region from the interface to the carrier 14 is precise, the gas permeability is lowered but the distance through which the gas should pass is made to be a half, the gas permeability as a whole is improved. Meanwhile, protons and electrons produced permeability from the exchange membrane 11 are led to outside through the conductive single body 14 and since the carrier 14 is precise, protons and electrons easily reach the interface of both carriers 14,



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15 and the conductivity as a whole is also improved as same as the gas permeability.

LEGAL STATUS

[Date of request for examination] 10.02.2003

[Date of sending the examiner's decision of rejection]

[Kind of final disposal of application other than the examiner's decision of rejection or application converted registration]

[Date of final disposal for application]

[Patent number] 3755840

[Date of registration] 06.01.2006

[Number of appeal against examiner's decision of rejection]

[Date of requesting appeal against examiner's decision of rejection]

[Date of extinction of right]

(19)日本国特許庁 (JP)

(12) 公開特許公報 (A)

(11)特許出願公開番号

特開平9-245802

(43)公開日 平成9年(1997)9月19日

(51)Int.Cl^{*}H01M
4/86
8/02
8/10

類別記号

序内整理番号

P I

H01M
4/86
8/02
8/10

技術表示箇所

M
P

審査請求 未請求 請求項の数 5 FD (全 7 頁)

(21)出願番号

特願平8-82106

(22)出願日

平成8年(1996)3月11日

(71)出願人 000217228

田中貴金属工業株式会社
東京都中央区日本橋茅場町2丁目6番6号

(71)出願人 000218166

辻邊 政廣
山梨県甲府市和田町2421番地の8

(74)代理人 弁理士 森 浩之

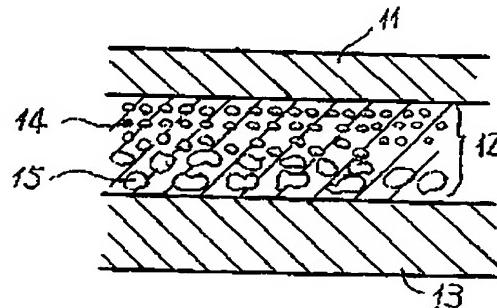
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(54)【発明の名称】高分子固体電解質型燃料電池用電極

(57)【要約】

【目的】従来の燃料電池では、ガス透過性とプロトン等の導伝性という相反する性能を高レベルで有しないため、満足できる高性能の燃料電池は存在しない。本発明は、従来の燃料電池用触媒層より高性能の触媒層を有する燃料電池用電極を提供することを目的とする。

【構成】触媒層12をイオン交換膜11とガス拡散層13で挟んで成る燃料電池の前記触媒層をイオン交換膜側の微孔の触媒担体14とガス拡散層側の多孔質の触媒担体15で構成する等して、触媒層の性能を該触媒層の厚さ方向に異ならせる。



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【特許請求の範囲】

【請求項 1】 脱媒が担持された触媒担体とイオン交換樹脂、又は触媒が担持された触媒担体とイオン交換樹脂と撥水性樹脂とを含む触媒層が、イオン交換膜とガス拡散層間に形成された高分子固体電解質型燃料電池用電極において、前記触媒層の性能を該触媒層の厚さ方向に異ならせたことを特徴とする高分子固体電解質型燃料電池用電極。

【請求項 2】 前記性能がイオン交換樹脂濃度であり、触媒層のイオン交換膜側に高濃度のイオン交換樹脂を使用し、ガス拡散層側に低濃度のイオン交換樹脂を使用する請求項1記載の高分子固体電解質型燃料電池用電極。

【請求項 3】 前記性能が触媒担体の比表面積であり、触媒層のイオン交換膜側に比表面積の小さい触媒担体を使用し、ガス拡散層側に比表面積の大きな触媒担体を使用する請求項1記載の高分子固体電解質型燃料電池用電極。

【請求項 4】 前記性能が触媒担体の緻密性であり、イオン交換膜側に緻密な触媒担体を使用し、ガス拡散層側に多孔質の触媒担体を使用する請求項1記載の高分子固体電解質型燃料電池用電極。

【請求項 5】 前記性能が触媒層であり、イオン交換膜側の触媒層を多くし、ガス拡散層側の触媒層を小さくした請求項1記載の高分子固体電解質型燃料電池用電極。

【発明の詳細な説明】

【0001】

【発明の属する技術分野】本発明は、高分子固体電解質型燃料電池用電極に関し、より詳細には触媒層とガス拡散層から成る燃料電池用電極における前記触媒層の性能向上させた前記燃料電池用電極に関する。

【0002】

【従来技術及び問題点】燃料電池は、水素や各種化石燃料を用いる高効率、無公害発電装置であることから、エネルギー問題、全地球的公害問題に対応できる。“ボストン原子力”的発電装置として、社会的に大きな期待が寄せられている。火力代替発電用、ビルディングや工場単位のオンラインサイト発電用、あるいは宇宙用など、用途に応じた各種燃料電池が開発されている。近年、炭酸ガスを中心とする温室効果や、NO_x、SO_x等による酸性雨が地球の将来を脅かす深刻な公害として認識されてきた。これら公害ガスの主要な排出源の一つが自動車等の内燃機関であることから、燃料電池を車載用内燃機関に代えて作動するモータ電源として利用する気運が急速に高まりつつある。この場合、多くの付帯設備と同様、電池は可能な限り小型であることが望ましく、そのためには電池本体の出力密度、出力電流密度が高いことが必須である。この条件を満たす有力な燃料電池の候補として、イオン交換膜を用いた高分子固体電解質型燃料電池（以下PEMFCという）が注目されている。

【0003】ここでPEMFCの本体の基本構造と作

用、問題点について説明する。図1に示す如く、PEM 1の両側に4A、4Cで示されるアノード及びカソードがホットプレスにより接合されることにより電池の基本が構成される。このアノード及びカソードは2A又は2Cで示される多孔質触媒層と3A又は3Cで示されるカーボンペーパーなどガス並散層からなる。電極反応は2A及び2C部の触媒表面で起こる。アノード反応ガス（H₂）は反応ガス供給孔5Aから3Aを通して供給され、カソード反応ガス（O₂）は反応ガス供給孔5Cから3Cを通して供給される。2A中では、アノード反応：H₂ → 2H⁺ + 2e⁻が、2C中ではカソード反応：1/2O₂ + 2H⁺ + 2e⁻ → H₂Oの反応が起こり、電池全体ではこれらの反応のトータルとしてH₂ + 1/2O₂ → H₂O + Q（反応熱）が起こる。この過程で起電力が得られ、この電気エネルギーにより外部負荷8を電子が流れる際に電気的仕事がなされる。

【0004】燃料電池の反応は前記触媒上で起こり、どのようにして前記触媒を有効利用するか、換言すると触媒層の性能ひいては燃料電池の性能を向上させるかが、20前記燃料電池により得られるエネルギー量を左右する最大の要因である。しかしながら従来の燃料電池では種々の理由により触媒層の性能を最大にすることはできず、高価な触媒特に白金族金属触媒を有効利用できていないという欠点がある。本発明者らはこの燃料電池の性能を最大にすることができない理由を検討した結果、その理由の1つが触媒層が均一であるためであることを見出した。従来から高分子固体電解質型燃料電池用電極の触媒層は、触媒とイオン交換樹脂、又は触媒とイオン交換樹脂と撥水性樹脂を、有機溶媒と水との混合液に懸濁した懸濁液を、電極基板上に一度に塗布し、乾燥し、焼成を行なって製造されている。この方法では一度に塗布を行なうため、触媒層の厚み方向で、触媒層の混成原料を変えることができず、触媒層の厚み方向でそれぞれに応じた最適な触媒層を得ることができない。触媒層の主要な機能はアノード及びカソードで生ずるプロトン及び電子を導伝して燃料電池反応を促進する点にある。一方触媒層は反応ガスを供給し、生成ガスを排出するという機能も有し、同じ触媒層でも反応サイトから離れるほど反応を促進しプロトンを導伝する機能よりもガス流通を円滑にする機能の方が直視されるようになる。しかし従来の触媒層は前述の通り均一でありそのガス流通の円滑性を与える触媒担体の緻密性も均一である。

【0005】このガス流通を円滑にする機能つまりガス透過性とプロトン（電子）導伝性とは二律背反的関係にあり、一方を高めると他方が低くなり、従来技術では両者を高めることは不可能である。従来の燃料電池は、前述した通り製造した電極（アノード及びカソード）2枚でイオン交換膜を挟み、これらをホットプレスで結着して製造されている。この方法では球形に近い形状の触媒担体がほぼ隙間なく充填されしかもホットプレスにより

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互いに強固に密着して密度が高くなりガス流通路が十分に形成されず、ガス透過性が大きく損なわれている。燃料電池反応は燃料ガスが反応サイトに供給されなければ生じないため、触媒活性がいかにも高くても燃料ガスが反応サイトに供給されなければ反応は生じない。従ってガス透過性は触媒活性より重要であるという見方も可能であり、ガス透過性の向上に対する考慮が殆どない従来の燃料電池はその触媒活性が十分に生かされていないとも言える。更に触媒層のうちイオン交換膜に近接する箇所ほど燃料電池反応への寄与が大きく触媒の利用率が高くなりガス拡散層に近接するほど触媒の利用率は低下するが、従来の触媒層が均一な燃料電池ではこの触媒利用率をより以上に向上させて最適化で燃料電池を運転するという考え方には存在しない。

【0006】

【発明が解決しようとする課題】そこで本発明は、触媒層の厚み方向にその機能、例えばイオン交換制脂濃度、触媒濃度、触媒担体の緻密性及び触媒担体の比表面積等を変化させることにより燃料電池の触媒層のガス透過性とプロトン導伝性という相反した関係にある両機能をそれぞれ向上させた燃料電池を提供することを目的とする。

【0007】

【課題を解決するための手段】上記の課題を解決するための本発明は、触媒が担持された触媒担体とイオン交換制脂、又は触媒が担持された触媒担体とイオン交換制脂と撥水性樹脂による触媒層が、イオン交換膜とガス拡散層間に形成された高分子固体電解質型燃料電池用電極において、前記触媒層の性能を該触媒層の厚さ方向に異ならせたことを特徴とする高分子固体電解質型燃料電池用電極である。前記性能としては、イオン交換制脂濃度、触媒担体の比表面積あるいは緻密性及び触媒濃度等がある。なお該性能は触媒層のイオン交換膜側からガス拡散層側に均一勾配で変化する必要はない。触媒層のイオン交換膜側の性能が全体としてガス拡散層側の性能と異なっていれば良い。

【0008】以下本発明を詳細に説明する。前述した通り燃料電池では、ガス拡散層側から燃料ガスを供給し該燃料ガスがガス拡散層を通過し更に触媒層を通過してイオン交換膜表面に達して反応が進行する。この反応はアノードでは水素ガスの酸化によるプロトン発生であり、カソードでは酸素ガスの還元による電子の発生である。アノード（カソード）で発生するプロトン（電子）は触媒層からガス拡散層を経て導線によりカソード（アノード）に接続された負荷を通ることにより初めて外部にエネルギーとして取り出される。従って触媒層の機能の1つであるプロトン（電子）導伝性から見ると、該機能を有するイオン交換制脂が担持された触媒担体は緻密であることが望ましい。しかし触媒層の他の機能であるガス透過性の観点からは前記触媒担体は多孔質であることが

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望ましい。

【0009】つまり触媒担体の緻密性に関して言えば、触媒層全体に亘って触媒担体の緻密性が均一であることは前述のガス透過性とプロトン（電子）導伝性の两者とともに向上させる観点からは望ましいことではない。従って本発明では、触媒担体の緻密性を触媒層の厚み方向に異ならせることにより、通常は二律背反的関係にある触媒層の主要性能であるガス透過性とプロトン（電子）導伝性をそれぞれ向上させることを可能にしている。つまり本発明では、燃料電池のイオン交換膜とガス拡散層間に配置された触媒層のイオン交換膜側に緻密な触媒担体をガス拡散層側に多孔質の触媒担体を配置し、前記緻密な触媒担体の触媒活性に優れた性能を反応サイトであるイオン交換膜近傍において十分に発揮させ、一方ガス拡散層側に多孔質の触媒担体を配置することにより、特に触媒層のガス拡散層側で要求されるガス透過性を向上させるようとしている。更に本発明では多孔質触媒担体を使用するため、該触媒担体がホットプレス等によっても完全に構成されることなくガス流通路が確保され、過度のガス透過性の低下がない。好ましい触媒担体の緻密性例えば一次粒子径はイオン交換膜側が100～300 Å、ガス拡散層側が300 Å～1 μmである。

【0010】図2は、この触媒層の厚み方向で触媒担体の緻密性を異ならせた燃料電池の電極を示すものである。図の電極は、上側から順にイオン交換膜11、触媒層12及びガス拡散層13の順に積層され、触媒層12のうちイオン交換膜11側は緻密な触媒担体14により、又ガス拡散層13側は多孔質の触媒担体15により構成されている。この電極にはガス拡散層13の下方から水素や酸素の燃料ガスが供給され、イオン交換膜11からは生成するプロトン（電子）及び生成ガスが取り出される。ガス拡散層13側から供給される燃料ガスは該ガス拡散層13側の触媒担体15が多孔質であるためその間を容易に通過して西触媒担体14、15の界面まで達する。この界面からイオン交換膜11側の触媒担体14は緻密であるためガス透過性は低下するが、透過すべき距離が半分になっているため、全体としてはガス透過能が改善される。

【0011】一方イオン交換膜11近傍の反応サイトで生成するプロトン（電子）は導伝性を有するカーボン等の触媒担体を介して外部の導線に取り出されるが、触媒層12のイオン交換膜11側の触媒担体14が緻密でありつまり導伝性濃度が高いため、容易に前記西触媒担体14、15の界面まで達する。この界面からガス拡散層13側の触媒担体15は多孔質であるため導伝性は低下するが、導伝されるべき距離が半分になっているため、全体としては導伝性が改善される。更に前記反応サイトで生成するガスも前記触媒層12を通過して取り出されるが、この場合にもガス拡散層13側の多孔質触媒担体15のため、全体のガス透過性が向上する。このような触媒層の厚み方向で異なる性質は触媒担体の多孔度に規定される訳ではなく、

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その他に触媒担体の比表面積、イオン交換樹脂量及び触媒濃度等の性質を触媒層の厚み方向で異ならせても良い。

【0012】触媒担体の比表面積の触媒活性やガス透過性に対する影響は画一的には決定できないが、触媒担体の粒径が一定の場合に比表面積を増加させると、換言すると担体の細孔を増加させると、ガス流通路が増加してガス透過性が向上しかつ担体の連続性が損なわれるためプロトン（電子）導伝性は低下する。逆に触媒担体の粒径が一定の場合に比表面積を減少させると、換言すると担体の細孔を減少させるとガス流通路が減少してガス透過性が低下しかつ担体のプロトン（電子）導伝性が増加する。従ってイオン交換膜側の触媒担体の比表面積を小さくしがガス拡散層側の触媒担体の比表面積を大きくすることにより、ガス透過性を高く維持しかつ反応活性も高い燃料電池を提供できる。好ましい触媒担体の比表面積はガス拡散層側が $250 \sim 2000 \text{ m}^2/\text{g}$ であり、イオン交換樹脂側が $50 \sim 400 \text{ m}^2/\text{g}$ である。次に触媒担体や防水性樹脂（例えばポリテトラフルオロエチレンやフッ素化ポリエチレンーポリプロピレン）とともに触媒層を構成するイオン交換樹脂は、プロトン（電子）の導伝性向上に寄与し、逆にガス透過性を低下させる。従って前記イオン交換樹脂濃度はイオン交換膜側で高くし、ガス拡散層側で低くすることにより、プロトン（電子）導伝性及びガス透過性の両者を高く維持できる。好ましいイオン交換樹脂濃度はガス拡散層側が $20 \sim 50\%$ 、イオン交換樹脂側が $40 \sim 70\%$ である。

【0013】図3は、この触媒層の厚み方向でイオン交換膜を異ならせた燃料電池の電極を示すものである。図の電極は、上側から順にイオン交換膜21、触媒層22及びガス拡散層23の順に積層され、触媒層22のうちイオン交換膜21側は担持されるイオン交換樹脂量が多い触媒担体24により、又ガス拡散層23側は担持されるイオン交換樹脂量が少ない触媒担体25により構成されている。この電極でも図2と同様にガス供給及びガス排出が行なわれ、ガス拡散層23側から供給される燃料ガスは該ガス拡散層23側の触媒担体25のイオン交換樹脂量が少ないとため担体間を容易に通過して両触媒担体24、25の界面まで達する。この界面からイオン交換膜21側の触媒担体24はイオン交換樹脂量が多いためガス透過能は低下するが、透過すべき距離が半分になっているため、全体としてはガス透過能が改善される。又図2の場合と同様に、イオン交換膜21近傍の反応サイトで生成するプロトン（電子）及び生成ガスの取り出しあら全体として改善される。

【0014】前述の触媒濃度を異ならせる場合も図3と同じように、イオン交換膜に近い側の触媒担体の触媒担持量を増加させ、ガス拡散層に近い側の触媒担体の触媒担持量を減少させて燃料電池用電極を構成する。好ましい触媒特に貴金属触媒の触媒担体に対する濃度はイオン交換膜側が $30 \sim 60\%$ 、ガス拡散層側が $10 \sim 40\%$ である。

である。この場合にはガス透過性に関する改善は生じないが、反応サイトに近い触媒濃度が高いため触媒利用率が向上し、全体的な触媒活性が増加する。前述した厚み方向に性能を異ならせた触媒層は、例えばガス並散層表面に、異なる混合比率（組成）又は原料を用いた懸濁液を複数回塗りましくは2～10回塗布を繰り返すことにより、又は別個に調製した性能の異なる複数の触媒層前駆体を接合することにより得られる。一回の塗布で形成される薄膜の厚さは特に限定されないがら $\sim 20 \mu\text{m}$ であることが好ましく、熱処理を行なう場合には、 $130 \sim 180^\circ\text{C}$ で $10 \sim 30 \text{ kg}/\text{cm}^2$ の圧でホットプレスすれば良い。

【0015】

【実施例】本発明の高分子固体電解質型燃料電池用電極の実施例を比較例とともに説明するが、これらは本発明を限定するものではない。

【実施例1】白金を $1 \text{ mg}/\text{cm}^2$ 担持した（カーボン担体に対して30重量%）、比表面積 $300 \text{ m}^2/\text{g}$ のカーボン担体を準備した。このカーボン担体3枚を、それぞれ該カーボン担体に対する重量比が58.5%、50%及び38.5%であるイオン交換樹脂（ナフィオン、デュポン社の商品名）5%溶液の懸濁液20gと蒸留水6gとともに遊星ボールミルにて50分間混合してペーストを得た。イオン交換樹脂濃度が38.5%であるペーストを、30重量%の防水性樹脂ポリテトラフルオロエチレンで防水化処理したカーボンペーパーから成るガス拡散層へ塗布し、 60°C で10分間乾燥し、更に 130°C 、 $20 \text{ kg}/\text{cm}^2$ で1分間焼成し、次にイオン交換樹脂濃度が50%であるペーストを同一条件で前記ペースト上へ塗布しつかし焼成し、更にイオン交換樹脂濃度が58.5%であるペーストを同一条件で前記ペースト上へ塗布しつかし焼成して前記ガス拡散層上へ触媒層を形成して電極とした（電極面積 $\pi \text{ cm}^2$ ）。

【0016】

【実施例2】カーボン担体として粒径 $0.03 \mu\text{m}$ 、表面積 $1300 \text{ m}^2/\text{g}$ のものを使用した。イオン交換樹脂のカーボン担体に対する重量比を50%とし、白金担持量が50重量%である実施例1と同じペーストを次いで白金担持量が40重量%である実施例1と同じペーストをガス拡散層へ塗布し、それぞれ 60°C で10分間乾燥し、更に 130°C 、 $20 \text{ kg}/\text{cm}^2$ で1分間焼成して触媒濃度が触媒層の厚み方向に異なる電極を製造した（電極面積 $\pi \text{ cm}^2$ ）。

【0017】

【比較例1】触媒層を、イオン交換樹脂の重量比がカーボン担体に対して50%である均一な触媒層としたこと以外は実施例1と同一条件でガス拡散層上へ触媒層を形成して電極とした。

【0018】上記のように製造された実施例1及びF2の電極と比較例1の電極各2枚でイオン交換膜（デュポン社製ナフィオン112）を挟み、それぞれセル温度 85°C 、 $350 \text{ ml}/\text{min}$ で水蒸ガスを $250 \text{ ml}/\text{min}$ で酸素ガスを供給しながら、電圧と電流密度の関係を測定したところ、図4

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のグラフに示すような結果を得た。このグラフから、実施例1及び実施例2の電極は高電流密度領域で比較例1の電流よりも高電圧を得ることができ、特に実施例2（イオン交換樹脂濃度を異ならせた電極）の電極の方が実施例1（触媒導通度を異ならせた電極）よりも良好な効果が生じたことが判る。

【0019】

【実施例3】ガス拡散層側の担体として白金を40重量%担持した（白金量は 0.5 mg/cm^2 ）比表面積が約 $1300 \text{ m}^2/\text{g}$ のカーボン担体を、又イオン交換樹脂側の担体として白金を40重量%担持した（白金量は 0.5 mg/cm^2 ）比表面積が約 $300 \text{ m}^2/\text{g}$ のカーボン担体をそれぞれ使用して、実施例1と同様にして電極を製造した（電極面積 $\pi \text{ cm}^2$ ）。

【0020】

【比較例2】触媒層を、イオン交換樹脂の重量比がカーボン担体に対して50%であり、白金を30重量%担持した（白金量は 1 mg/cm^2 ）比表面積が約 $300 \text{ m}^2/\text{g}$ のカーボン担体を使用して構成し、均一な触媒層を有する電極を製造した（電極面積 $\pi \text{ cm}^2$ ）。

【0021】上記のように製造された実施例3と比較例2の電極各2枚でイオン交換膜（デュポン社製ナフィオン112）を挟み、それぞれセル温度 80°C 、 $350 \text{ mL}/\text{分}$ で水素ガスを $250 \text{ mL}/\text{分}$ で酸素ガスを供給しながら、電圧と電流密度の関係を測定したところ、図5のグラフに示すような結果を得た。このグラフから、実施例3の電極は高電流密度領域で比較例2の電流よりも高電圧を得ることができたことが判る。

【0022】

【実施例4】ガス拡散層側の担体として、粒径 $0.03 \mu \text{m}$ 、表面積 $1300 \text{ m}^2/\text{g}$ のものを使用し、イオン交換膜側の担体として、粒径 $0.015 \mu \text{m}$ 、表面積 $1500 \text{ m}^2/\text{g}$ のものを使用し、白金を40重量%担持して（白金量は 1 mg/cm^2 ）電極面積が $\pi \text{ cm}^2$ である電極を製造した。この電極を使用して、上述の実施例1と同一条件で電圧と電流密度の関係を測定したところ、図6のグラフに示すような結果を得た。このグラフから、高電流密度領域でも比較的高い電圧でエネルギーを取り出せたことが判る。

【0023】

【発明の効果】本発明は、触媒が担持された触媒担体とイオン交換樹脂、又は触媒が担持された触媒担体とイオン交換樹脂と撥水性樹脂による触媒層が、イオン交換膜とガス拡散層間に形成された高分子固体電解質型燃料電池用電極において、前記触媒層の性能を該触媒層の厚さ方向に異ならせることと特徴とする高分子固体電解質型燃料電池用電極である（請求項1）。燃料電池の触媒層はガス透過性とプロトン（電子）導伝性という相反した性能を要求されるが、従来の燃料電池では比較的緻密な触媒担体やイオン交換樹脂をホットプレス等で結着して製造されている。この製法では球形に近い形状の触媒担体がほぼ隙間なく充填されしかもホットプレスにより互

いに強固に密着して密度が高くなりガス流通路は殆ど形成されず、ガス透過性が大きく損なわれている。

【0024】つまり従来の燃料電池では、燃料電池の触媒層の主たる機能であるガス透過性とプロトン等の導伝性のうち、ガス透過性を犠牲にしてプロトン等の導伝性を向上させることを意図している。しかしながら燃料ガスが反応サイトに供給され生成ガスが取り出されない限り反応は進行しない。従って従来の燃料電池では反応が十分遠く進行せず、燃料電池の特性であるエネルギー生成が不十分となっている。この欠点を解消するために前記ホットプレスによる結合を弱くするとプロトン等の導伝性が損なわれ、ガスの供給及び排出は円滑に行なわれても、プロトン等の移動によるエネルギー生成が損なわれる。

【0025】前述の本発明では、触媒層の性能を該触媒層の厚さ方向に異ならせることにより、触媒層のイオン交換樹脂側とガス拡散層側でその主として達成される性能を相違させることにより、例えば前述のガス透過性及びプロトン等の導伝性に優れた燃料電池用電極を提供できる。この前記触媒層の厚み方向に異ならせる性能としては、第1にイオン交換樹脂濃度がある（請求項2）。イオン交換樹脂濃度が高いとプロトン等の導伝性は高くなるがガス透過性は低下する。従ってプロトン等の導伝性を必要とする触媒層のイオン交換樹脂側ではイオン交換樹脂濃度を高くし、プロトン等の導伝性をさほど必要とせず、むしろガス透過性を必要とする触媒層のガス透過性側ではイオン交換樹脂濃度を低くし、換言すると触媒層の厚み方向にイオン交換樹脂濃度の勾配を形成することにより、ガス透過性とプロトン等の導伝性に優れた燃料電池用電極を提供できる。

【0026】前述の触媒層の厚み方向に異ならせる性能としては、第2に触媒担体の比表面積がある（請求項3）。触媒担体の粒径が一定の場合に比表面積を増加させると、換言すると担体の細孔を増加させると、ガス流通路が増加してガス透過性が向上しつつ担体の連続性が損なわれるためプロトン等の導伝性は低下する。逆に触媒担体の粒径が一定の場合に比表面積を減少させると、換言すると担体の細孔を減少させるとガス流通路が減少してガス透過性が低下しつつ担体のプロトン等の導伝性が増加する。従って触媒層のイオン交換膜側の触媒担体の比表面積を小さくしガス拡散層側の触媒担体の比表面積を大きくすることにより、ガス透過性を高く維持しつつ反応活性も高い燃料電池を提供できる。

【0027】前述の触媒層の厚さ方向に異ならせる性能としては、第3に触媒担体の微孔性がある（請求項4）。触媒担体の微孔性が高いとプロトン等の導伝性は高くなる反面、ガス透過性は大きく減少する。従ってイオン交換膜側の触媒担体として微孔性触媒担体を、ガス透過性の触媒担体として多孔質の触媒担体を使用することにより、ガス透過性及びプロトン等の導伝性とも優れ

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た燃料電池用電極を提供できる。前述の触媒層の厚さ方向に異ならせる最後の性能として触媒層（濃度）がある（請求項5）。燃料電池の反応は触媒層のイオン交換膜側で主として起こるため、触媒層のうちイオン交換膜側の触媒濃度を高くしたままガス拡散層側の触媒濃度を減少させても実質的な触媒活性が低下することなく、使用する高価な触媒を低減させることができる。

【図面の簡単な説明】

【図1】従来のイオン交換膜を使用した燃料電池の基本構造を示す概略図。

【図2】本発明の高分子固体電解質型燃料電池用電極の一実施例を示す断面図。

【図3】本発明の高分子固体電解質型燃料電池用電極の*

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*他の実施例を示す断面図。

【図4】実施例1、2及び比較例1における電流密度と電圧の関係を示すグラフ。

【図5】実施例3及び比較例2における電流密度と電圧の関係を示すグラフ。

【図6】実施例4における電流密度と電圧の関係を示すグラフ。

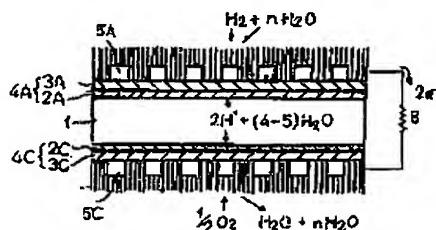
【符号の説明】

11, 21···イオン交換膜 12, 22···触媒層 1

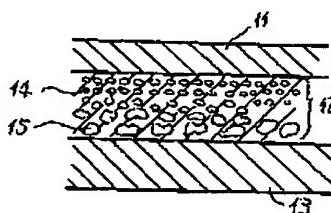
13, 23···ガス拡散層

14, 24···イオン交換膜側触媒担体 15, 25···ガス拡散層側触媒担体

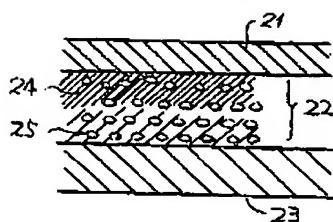
【図1】



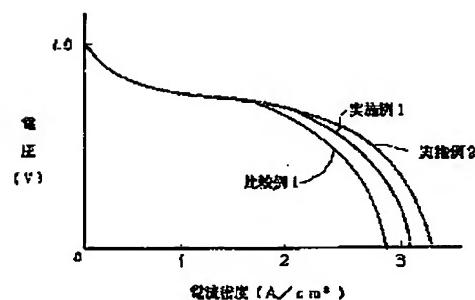
【図2】



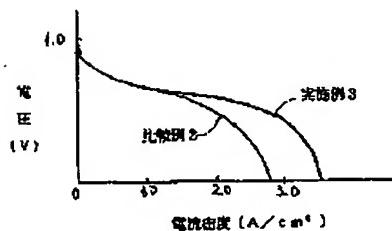
【図3】



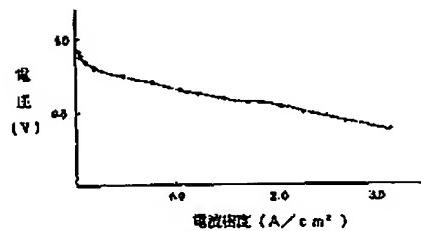
【図4】



【図5】



【図6】



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フロントページの続き

(71)出願人 391016716
ストンハルト・アソシエーツ・インコーポ
レーテッド
STONEHART ASSOCIATE
S INCORPORATED
アメリカ合衆国 06443 コネチカット州、
マジンン、コティッジ・ロード17、ビー・オ
ー・ボックス1220

(72)発明者 多田 智之
神奈川県平塚市新町2番73号 因中貴金属
工業株式会社技術開発センター内
(72)発明者 戸島 康仁
神奈川県平塚市新町2番73号 因中貴金属
工業株式会社技術開発センター内
(72)発明者 只野 銀子
神奈川県平塚市新町2番73号 因中貴金属
工業株式会社技術開発センター内

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention relates to said electrode for fuel cells which raised more the engine performance of said catalyst bed in the electrode for fuel cells which changes from a catalyst bed and a gaseous diffusion layer to a detail about the electrode for solid polymer mold fuel cells.

[0002]

[The conventional technique and a trouble] Since a fuel cell is efficient and the pollution-free power plant which use hydrogen and various fossil fuels, it has a great hope socially as a power plant of "postatomic energy" which can cope with energy problems and a full-terrestrial pollution problem. Various fuel cells according to an application, such as an object for a steam-generated alternative generation of electrical energy, an object for the on-site power generation of a building or a works unit, or an object for space, are developed. In recent years, the acid rain by the greenhouse effect centering on carbon dioxide gas, NOx, SOx, etc. is recognized as a serious public nuisance which threatens the future of the earth. Since one of the main sources of discharge of these public nuisance gas is internal combustion engines, such as an automobile, the tendency which uses a fuel cell as a motor power source which replaces with the internal combustion engine for mount, and operates is increasing quickly. In this case, like much equipment, the thing of a cell small as much as possible is desirable, and it is indispensable that the power density of a cell proper and an output current consistency are high for that purpose. The solid polymer electrolyte mold fuel cell (it is called Following PEMFC) using ion exchange membrane as a candidate of a leading fuel cell who fulfills this condition attracts attention.

[0003] The basic structure of the body of PEMFC, an operation, and a trouble are explained here. As shown in drawing 1, the base of a cell is constituted by joining the anode and cathode which are shown by 4A and 4C by the hotpress to the both sides of PEM1. This anode and cathode consist of gaseous diffusion layers, such as carbon paper shown by the porosity catalyst bed, 3A, or 3C shown by 2A or 2C. Electrode reaction occurs on the catalyst front face of 2A and 2C sections. Anode reaction gas (H₂) is supplied through reactant gas feed-holes 5A to 3A, and cathode reaction gas (O₂) is supplied through reactant gas feed-holes 5C to 3C. In 2A, it is anode reaction:H₂ ->2H++2e. - In 2C, it is a cathode reaction. : The reaction of 1/2O₂+2H++2e-->H₂O occurs, and H₂+1 / 2O₂ ->H₂O+Q (heat of reaction) happens as these reactions being total by the whole cell. Electromotive force is acquired in this process, and electric work is made in case an electron flows the external load 8 with this electrical energy.

[0004] How said catalyst is used effectively by the reaction of a fuel cell occurring on said catalyst or whether if it puts in another way, **** of a catalyst bed, as a result the engine performance of a fuel cell will be raised are the greatest factor which influences the amount of energy obtained by said fuel cell. However, in the conventional fuel cell, the engine performance of a catalyst bed cannot be made into max for various reasons, but there is a fault that the expensive catalyst, especially the platinum metal catalyst cannot be used effectively. this invention persons found out that one of the reason of that was because the catalyst bed is uniform, as a result of considering carefully the reason which cannot make the engine performance of this fuel cell max. From the former, the catalyst bed of the electrode for solid polymer electrolyte mold fuel cells applies at once the suspension which ****(ed) a catalyst, ion exchange resin or a catalyst and ion exchange resin, and water-repellent resin into the mixed liquor of an organic solvent and water on an electrode substrate, it dries, and calcinates and is manufactured. In this approach, since it applies at once, the hybrid raw material of a catalyst bed cannot be changed in the thickness direction of a catalyst bed, and the optimal catalyst bed according to each cannot be obtained in the thickness direction of a catalyst bed. The main functions of a catalyst bed are in the point which **** the proton and electron which are produced with an

anode and a cathode, and promotes a fuel cell reaction. On the other hand, a catalyst bed supplies reactant gas and it also has the function to discharge generation gas, and greater importance comes to be attached than to the function to promote a reaction and to **** a proton, to the function which makes gas circulation smooth, so that the same catalyst bed also separates from a reaction site. However, the conventional catalyst bed is uniform as above-mentioned, and its compactness of the catalyst support which gives the smooth nature of the gas circulation is also uniform.

[0005] It has an antinomy-relation, if one side is raised, another side will become low, and the function, i.e., gas permeability, which makes this gas circulation smooth, and proton (electron) conductivity cannot raise both with the conventional technique. Ion exchange membrane of the conventional fuel cell is pinched with two electrodes (an anode and cathode) manufactured as mentioned above, and it binds these with a hotpress and is manufactured. The catalyst support of the configuration near a globular form is filled up with this approach that there is almost no clearance, moreover, it sticks firmly mutually with a hotpress, a consistency becomes high, and a gas circulation way is not fully formed, but gas permeability is spoiled greatly. Since a fuel cell reaction is not produced if fuel gas is not supplied to a reaction site, a reaction is not produced if fuel gas will not be supplied to a reaction site, however high catalytic activity may be. Therefore, the view that gas permeability is more important than catalytic activity is also possible, and the conventional fuel cell which does not almost have the consideration to the improvement in gas permeability can be said to be that the catalytic activity is not fully employed efficiently. Furthermore, the view of raising this catalyst utilization factor above more in a fuel cell with the conventional uniform catalyst bed although the utilization factor of a catalyst falls so that the contribution to a fuel cell reaction is as large as the part which approaches ion exchange membrane among catalyst beds and the utilization factor of a catalyst approaches a gaseous diffusion layer highly and conversely, and operating a fuel cell with an optimum value does not exist.

[0006]

[Problem(s) to be Solved by the Invention] Then, this invention aims at offering the fuel cell which raised both the functions that have a conflicting relation called the gas permeability of the catalyst bed of a fuel cell, and proton conductivity, respectively by changing the compactness of the function, for example, ion-exchange-resin concentration, catalyst concentration, and catalyst support, the specific surface area of catalyst support, etc. in the thickness direction of a catalyst bed.

[0007]

[Means for Solving the Problem] This invention for solving the above-mentioned technical problem is an electrode for solid polymer electrolyte mold fuel cells with which the catalyst bed by the catalyst support and ion exchange resin with which the catalyst was supported, or the catalyst support, the ion exchange resin and the water-repellent resin with which the catalyst was supported is characterized by changing the engine performance of said catalyst bed in the thickness direction of this catalyst bed in the electrode for solid polymer electrolyte mold fuel cells formed between ion exchange membrane and a gaseous diffusion layer. As said engine performance, there are specific surface area or compactness, catalyst concentration, etc. of ion-exchange-resin concentration and catalyst support. In addition, this engine performance does not need to change from the ion-exchange-membrane side of a catalyst bed to a gaseous diffusion layer side with homogeneity inclination, and the engine performance by the side of the ion exchange membrane of a catalyst bed should just differ from the engine performance by the side of a gaseous diffusion layer as a whole.

[0008] This invention is explained to a detail below. In a fuel cell, fuel gas is supplied from a gaseous diffusion layer side, this fuel gas penetrates a gaseous diffusion layer, a catalyst bed is penetrated further, an ion-exchange-membrane front face is arrived at, and a reaction advances as mentioned above. This reaction is proton generating by oxidation of hydrogen gas in an anode, and is generating of the electron by reduction of oxygen gas in a cathode. The proton (electron) generated with an anode (cathode) will not be taken out without passing along the load connected to the cathode (anode) by lead wire through the gaseous diffusion layer from the catalyst bed as energy outside. Therefore, when it sees from the proton (electron) conductivity which is one of the functions of a catalyst bed, the precise thing of the catalyst support with which the ion exchange resin which has this function was supported is desirable. However, as for said catalyst support, from a viewpoint of gas permeability which are other functions of a catalyst bed, it is desirable that it is porosity.

[0009] That is, if it says about the compactness of catalyst support, from a viewpoint which covers the whole catalyst bed and raises both gas permeability of the above-mentioned [that the compactness of catalyst support is uniform], and both proton (electron) conductivity, it will not be desirable. Therefore, in

this invention, it makes it possible to raise the gas permeability which is the major performance of the catalyst bed which usually has an antinomy-relation, and proton (electron) conductivity, respectively by changing the compactness of catalyst support in the thickness direction of a catalyst bed. That is, in this invention, porous catalyst support is arranged for catalyst support precise to the ion-exchange-membrane [of a fuel cell], and ion-exchange-membrane side of the catalyst bed arranged between gaseous diffusion layers to a gaseous diffusion layer side. He is trying to raise the gas permeability especially demanded by the gaseous diffusion layer side of a catalyst bed by fully demonstrating the engine performance excellent in the catalytic activity of said precise catalyst support [near / which is a reaction site / the ion exchange membrane], and on the other hand arranging porous catalyst support to a gaseous diffusion layer side. Furthermore, in order to use porosity catalyst support in this invention, this catalyst support is not completely crushed by a hotpress etc., a gas circulation way is secured, and too much fall of gas permeability cannot be found. An ion-exchange-membrane side is [a 100 - 300 ** and gaseous diffusion layer side] 300 **-1micrometer, the compactness of a primary particle, for example, the diameter, of desirable catalyst support.

[0010] Drawing 2 shows the electrode of the fuel cell which changed the compactness of catalyst support in the thickness direction of this catalyst bed. The laminating of the electrode of drawing is carried out to order from the bottom at the order of ion exchange membrane 11, a catalyst bed 12, and the gaseous diffusion layer 13, and the gaseous diffusion layer 13 side is constituted by the porous catalyst support 15 among catalyst beds 12 by the catalyst support 14 with a precise ion-exchange-membrane 11 side again. The fuel gas of hydrogen or oxygen is supplied to this electrode from the lower part of the gaseous diffusion layer 13, and the proton (electron) and generation gas to generate are taken out from ion exchange membrane 11. Since the catalyst support 15 by the side of this gaseous diffusion layer 13 is porosity, the fuel gas supplied from the gaseous diffusion layer 13 side passes the meantime easily, and attains it to the interface of both the catalyst support 14 and 15. From this interface, since the catalyst support 14 by the side of ion exchange membrane 11 is precise, gas penetrability falls, but since the distance which should be penetrated is half, gas penetrability is improved as the whole.

[0011] Although taken out by external lead wire through catalyst support, such as carbon which has conductivity, since [that the catalyst support 14 by the side of the ion exchange membrane 11 of a catalyst bed 12 is precise that is,] conductor concentration is high, the proton (electron) generated to an about 11-ion exchange membrane reaction site on the other hand is easily attained to the interface of said both catalyst support 14 and 15. From this interface, since the catalyst support 15 by the side of the gaseous diffusion layer 13 is porosity, conductivity falls, but since the distance which should be ****(ed) is half, conductivity is improved as the whole. Furthermore, although the gas generated to said reaction site is also taken out through said catalyst bed 12, the whole gas permeability improves also in this case for the porosity catalyst support 15 by the side of the gaseous diffusion layer 13. The property changed in the thickness direction of such a catalyst bed is not necessarily limited to the porosity of catalyst support, in addition may change properties, such as specific surface area of catalyst support, the amount of ion exchange resin, and catalyst concentration, in the thickness direction of a catalyst bed.

[0012] Although the effect to the catalytic activity of the specific surface area of catalyst support or gas permeability cannot be determined uniformly, if the pore of support is made to increase when it will put in another way, if specific surface area is made to increase when the particle size of catalyst support is fixed, since a gas circulation way increases, and gas permeability improves and the continuity of support is spoiled, proton (electron) conductivity will fall. Conversely, if specific surface area is decreased when the particle size of catalyst support is fixed, it will put in another way and the pore of support will be decreased, gas circulation ways will decrease in number, and gas permeability will fall, and the proton (electron) conductivity of support will increase. Therefore, by making small specific surface area of the catalyst support by the side of ion exchange membrane, and enlarging specific surface area of the catalyst support by the side of a gaseous diffusion layer, gas permeability is maintained highly and a fuel cell also with high labile can be offered. A gaseous diffusion layer side is 250-2000m²/g, and the ion-exchange-resin side of the specific surface area of desirable catalyst support is 50-400 m²/g. Next, it contributes to the improvement in conductive of a proton (electron), and the ion exchange resin which constitutes a catalyst bed with catalyst support and water-repellent resin (for example, polytetrafluoroethylene and fluorination polyethylene-polypropylene) reduces gas permeability conversely. Therefore, said ion-exchange-resin concentration can maintain highly both proton (electron) conductivity and gas permeability by making it high and making it low by the gaseous diffusion layer side by the ion-exchange-membrane side. A gaseous diffusion layer side is [the ion-exchange-resin side of desirable ion-exchange-resin concentration] 40 - 70

% of the weight 20 to 50% of the weight.

[0013] Drawing 3 shows the electrode of the fuel cell which changed the amount of ion exchange membrane in the thickness direction of this catalyst bed. The laminating of the electrode of drawing is carried out to order from the bottom at the order of ion exchange membrane 21, a catalyst bed 22, and the gaseous diffusion layer 23, and the gaseous diffusion layer 23 side is constituted again by the catalyst support 24 with many amounts of ion exchange resin with which an ion-exchange-membrane 21 side is supported among catalyst beds 22 by the catalyst support 25 with few amounts of ion exchange resin supported. Gas supply and gas discharge are performed like [this electrode] drawing 2 , and since the fuel gas supplied from the gaseous diffusion layer 23 side has few amounts of ion exchange resin of the catalyst support 25 by the side of this gaseous diffusion layer 23, it passes through between support easily and attains it to the interface of both the catalyst support 24 and 25. From this interface, since the catalyst support 24 by the side of ion exchange membrane 21 has many amounts of ion exchange resin, gas penetrability falls, but since the distance which should be penetrated is half, gas penetrability is improved as the whole. Moreover, the ejection of the proton (electron) generated to an about 21 ion exchange membrane reaction site and generation gas as well as the case of drawing 2 is improved as a whole.

[0014] As well as drawing 3 when it changes the above-mentioned catalyst concentration, the amount of catalyst support of the catalyst support of the side near ion exchange membrane is made to increase, the amount of catalyst support of the catalyst support of the side near a gaseous diffusion layer is decreased, and the electrode for fuel cells is constituted. An ion-exchange-membrane side is [the gaseous diffusion layer side of the concentration to the catalyst support of a desirable catalyst, especially a precious metal catalyst] 10 - 40 % of the weight 30 to 60% of the weight. In this case, although the improvement about gas permeability is not produced, since the catalyst concentration near a reaction site is high, a catalyst utilization factor improves, and overall catalytic activity increases. the mixing ratio from which the catalyst bed which changed the engine performance in the thickness direction mentioned above differs for example, on a gaseous diffusion layer front face -- the suspension using a rate (presentation) or a raw material -- multiple times -- repeating spreading 2 to 10 times desirably -- or it is obtained by joining two or more catalyst bed precursors with which the engine performance prepared separately differs. What is necessary is it to be desirable that it is 5-20 micrometers, although especially the thickness of the thin film formed by one spreading is not limited, and just to carry out the hotpress of it by 10-30kg/cm² ** by 130 - 180 **, in heat-treating.

[0015]

[Example] Although the example of the electrode for solid polymer electrolyte mold fuel cells of this invention is explained with the example of a comparison, these do not limit this invention.

[Example 1] The carbon support of specific-surface-area (it is 30 % of the weight to carbon support) 300 m²/g which supported platinum two times 1 mg/cm was prepared. Three sorts of these carbon support was mixed for 50 minutes with the planet ball mill with 20g of concentration liquid and 6g of distilled water of 5% (trade name of Nafion and Du Pont) solution of ion-exchange resin whose weight ratios to this carbon support are 58.5%, 50%, and 38.5%, respectively, and the paste was obtained. It applies to the gaseous diffusion layer which consists of the carbon paper which carried out water-repellent treatment of the paste whose ion-exchange-resin concentration is 38.5% by 30% of the weight of water-repellent resin polytetrafluoroethylene. Dry for 10 minutes at 60 degrees C, and also it calcinates for 1 minute by 130 ** and 20kg/cm². Next, apply the paste whose ion-exchange-resin concentration is 50% to up to the paper described above on the same conditions, and it is calcinated. Furthermore, on the same conditions, ion-exchange-resin concentration applied to up to said paste the paste which is 58.5%, and calcinates it, formed the catalyst bed in up to said gaseous diffusion layer, and considered as the electrode (electrode surface product picm²).

[0016]

[Example 2] The thing of the particle size of 0.03 micrometers and surface area of 1300m²/g was used as carbon support. The electrode with which the weight ratio to the carbon support of ion-exchange resin is made into 50%, the same paste as the example 1 whose amount of platinum support is 50 % of the weight, and the example 1 whose amount of platinum support is subsequently 40 % of the weight about the same paste is applied to a gaseous diffusion layer, and it dries for 10 minutes at 60 degrees C, respectively, and also it calcinates for 1 minute by 130 ** and 20kg/cm², and catalyst concentration differs in the thickness direction of a catalyst bed be manufactured (electrode surface product picm²)

[0017]

[The example 1 of a comparison] Except the weight ratio of ion-exchange resin having made the catalyst

bed the uniform catalyst bed which is 50% to carbon support, the catalyst bed was formed in up to a gaseous diffusion layer on the same conditions as an example 1, and it considered as the electrode.

[0018] When the relation between an electrical potential difference and current density was measured having supplied hydrogen gas by part for cel temperature [of 80 degrees C], and 350ml/, and supplying [pinched the ion exchange membrane (Du Pont Nafion 112) with the electrode of examples 1 and 2 and two electrodes each of the example 1 of a comparison which were manufactured as mentioned above,] oxygen gas by part for 250 ml/, respectively, the result as shown in the graph of drawing 4 was obtained. This graph shows that the electrode of an example 1 and an example 2 could obtain the high voltage rather than the current of the example 1 of a comparison in the high current density field, and the effectiveness with the electrode of an example 2 (electrode which changed ion-exchange-resin concentration) especially better than an example 1 (electrode which changed catalyst concentration) arose.

[0019]

[Example 3] The carbon support whose specific surface area (the amount of platinum is 0.5 mg/cm²) which supported platinum 40% of the weight as support by the side of a gaseous diffusion layer is about 1300m²/g Moreover, the carbon support whose specific surface area (the amount of platinum is 0.5 mg/cm²) which supported platinum 40% of the weight as support by the side of ion exchange membrane is abbreviation 300 m²/g was used, respectively, and the electrode was manufactured like the example 1 (electrode surface product picm²).

[0020]

[The example 2 of a comparison] About a catalyst bed, the weight ratio of ion-exchange resin is 50% to carbon support, the specific surface area (the amount of platinum is 1 mg/cm²) which supported platinum 30% of the weight constituted using the carbon support which is abbreviation 300 m²/g, and the electrode which has a uniform catalyst bed was manufactured (electrode surface product picm²).

[0021]

When the relation between an electrical potential difference and current density was measured having supplied hydrogen gas by part for cel temperature [of 80 degrees C], and 350 ml/, and supplying [pinched each the ion exchange membrane (Du Pont Nafion 112) with two electrodes of the example 3 manufactured as mentioned above and the example 2 of a comparison,] oxygen gas by part for 250 ml/, respectively, the result as shown in the graph of drawing 5 was obtained. This graph shows that the electrode of an example 3 was able to obtain the high voltage rather than the current of the example 2 of a comparison in the high current density field.

[0022]

[Example 4] as the support by the side of a gaseous diffusion layer -- the thing of the particle size of 0.03 micrometers, and surface area of 1300m²/g -- using it -- as the support by the side of ion exchange membrane -- particle size 0.015 the thing of mum and surface area of 1500m²/g -- using it -- platinum -- 40 % of the weight -- supporting -- an electrode surface (amount of platinum is 1 mg/cm²) product -- picm² it is -- the electrode was manufactured. When this electrode was used and the relation between an electrical potential difference and current density was measured on the same conditions as the above-mentioned example 1, the result as shown in the graph of drawing 6 was obtained. This graph shows that energy was able to be comparatively taken out by the high voltage also in the high current density field.

[0023]

[Effect of the Invention] It is the electrode for solid polymer electrolyte mold fuel cells characterized by this invention changing the engine performance of said catalyst bed in the thickness direction of this catalyst bed in the electrode for solid polymer electrolyte mold fuel cells with which the catalyst bed by the catalyst support and ion exchange resin with which the catalyst was supported, or the catalyst support, the ion exchange resin and the water-repellent resin with which the catalyst was supported was formed between ion exchange membrane and a gaseous diffusion layer (claim 1). Although the conflicting engine performance of gas permeability and proton (electron) conductivity is required of the catalyst bed of a fuel cell, with the conventional fuel cell, comparatively precise catalyst support and ion exchange resin are bound with a hotpress etc., and it is manufactured. The catalyst support of the configuration near a globular form is filled up with this process that there is almost no clearance, moreover, it sticks firmly mutually with a hotpress, and a consistency becomes high, most gas circulation ways are not formed but gas permeability is spoiled greatly.

[0024] That is, in the conventional fuel cell, it has the intention of raising conductivity, such as a proton, at the sacrifice of gas permeability among the gas permeability which is the main function of the catalyst bed of a fuel cell, and conductivity, such as a proton. However, unless fuel gas is supplied to a reaction site and generation gas is taken out, a reaction does not advance. Therefore, a reaction does not advance sufficiently

quickly but the conventional fuel cell of the energy generation which is the property of a fuel cell is inadequate. If binding by said hotpress is weakened in order to cancel this fault, even if conductivity, such as a proton, will be spoiled and supply and discharge of gas will be performed smoothly, the energy generation by migration of a proton etc. is spoiled.

[0025] In above-mentioned this invention, the electrode for fuel cells excellent in conductivity, such as the above-mentioned gas permeability and a proton, can be offered by making the engine performance mainly attained different by the ion-exchange-membrane [of a catalyst bed], and gaseous diffusion layer side by changing the engine performance of a catalyst bed in the thickness direction of this catalyst bed. As engine performance which makes it differ in the thickness direction of said this catalyst bed, ion-exchange-resin concentration is in the 1st (claim 2). If ion-exchange-resin concentration is high, although conductivity, such as a proton, will become high, gas permeability falls. Therefore, at the ion-exchange-membrane side of the catalyst bed which needs conductivity, such as a proton, by the gas permeability side of the catalyst bed which makes ion-exchange-resin concentration high, and does not need conductivity, such as a proton, so much, but needs gas permeability rather, if ion-exchange-resin concentration is made low and put in another way, the electrode for fuel cells excellent in gas permeability and conductivity, such as a proton, can be offered by forming the inclination of ion-exchange-resin concentration in the thickness direction of a catalyst bed.

[0026] There is [2nd] specific surface area of catalyst support as engine performance which makes it differ in the thickness direction of the above-mentioned catalyst bed (claim 3). If the pore of support is made to increase when it will put in another way, if specific surface area is made to increase when the particle size of catalyst support is fixed, since a gas circulation way increases, and gas permeability improves and the continuity of support is spoiled, conductivity, such as a proton, will fall. Conversely, if specific surface area is decreased when the particle size of catalyst support is fixed, it will put in another way and the pore of support will be decreased, gas circulation ways will decrease in number, and gas permeability will fall, and conductivity, such as a proton of support, will increase. Therefore, by making small specific surface area of the catalyst support by the side of the ion exchange membrane of a catalyst bed, and enlarging specific surface area of the catalyst support by the side of a gaseous diffusion layer, gas permeability is maintained highly and a fuel cell also with high labile can be offered.

[0027] There is [3rd] compactness of catalyst support as engine performance which makes it differ in the thickness direction of the above-mentioned catalyst bed (claim 4). If the compactness of catalyst support is high, while conductivity, such as a proton, will become high, gas permeability decreases greatly. Therefore, the electrode for fuel cells in which conductivity, such as gas permeability and a proton, was excellent by using porous catalyst support as catalyst support of gas permeability in catalyst support precise as catalyst support by the side of ion exchange membrane can be offered. There is the amount of catalysts (concentration) as engine performance of the last which makes it differ in the thickness direction of the above-mentioned catalyst bed (claim 5). Since the reaction of a fuel cell mainly occurs by the ion-exchange-membrane side of a catalyst bed, even if it decreases the catalyst concentration by the side of a gaseous diffusion layer, making high catalyst concentration by the side of ion exchange membrane among catalyst beds, the expensive amount of catalysts which substantial catalytic activity does not fall and is used can be reduced.

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CLAIMS

[Claim(s)]

[Claim 1] The electrode for solid polymer electrolyte mold fuel cells characterized by the catalyst bed containing the catalyst support and ion exchange resin with which the catalyst was supported or the catalyst support and ion exchange resin with which the catalyst was supported, and water-repellent resin changing the engine performance of said catalyst bed in the thickness direction of this catalyst bed in the electrode for solid polymer electrolyte mold fuel cells formed between ion exchange membrane and a gaseous diffusion layer.

[Claim 2] The electrode for solid polymer electrolyte mold fuel cells according to claim 1 which said engine performance is ion-exchange-resin concentration, and uses high-concentration ion exchange resin and uses low-concentration ion exchange resin for the ion-exchange-membrane side of a catalyst bed at a gaseous diffusion layer side.

[Claim 3] The electrode for solid polymer electrolyte mold fuel cells according to claim 1 which said engine performance is the specific surface area of catalyst support, uses catalyst support with a small specific surface area for the ion-exchange-membrane side of a catalyst bed, and uses catalyst support with a big specific surface area for a gaseous diffusion layer side.

[Claim 4] The electrode for solid polymer electrolyte mold fuel cells according to claim 1 which said engine performance is the compactness of catalyst support, uses precise catalyst support for an ion-exchange-membrane side, and uses porous catalyst support for a gaseous diffusion layer side.

[Claim 5] The electrode for solid polymer electrolyte mold fuel cells according to claim 1 which said engine performance is the amount of catalysts, made [many] the amount of catalysts by the side of ion exchange membrane, and made small the amount of catalysts by the side of a gaseous diffusion layer.

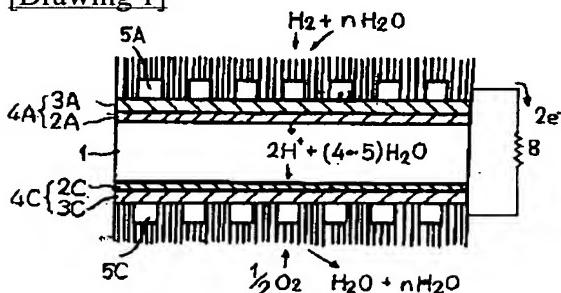
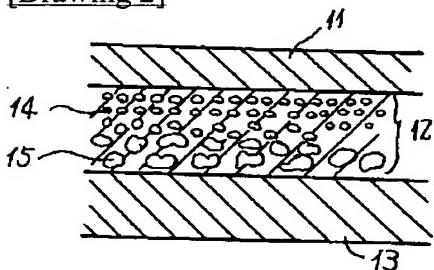
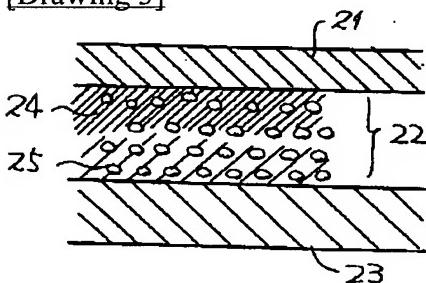
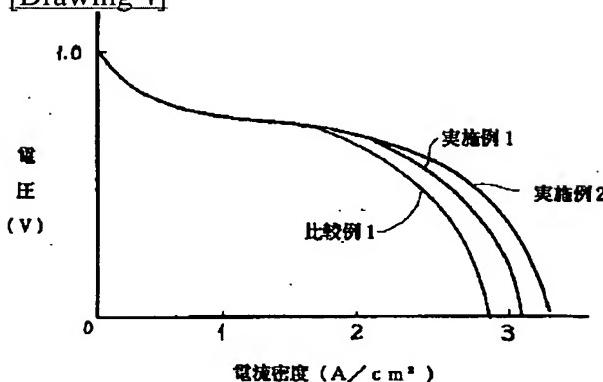
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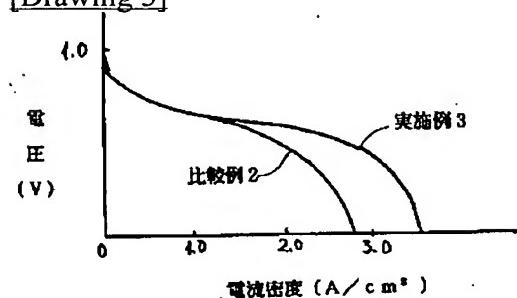
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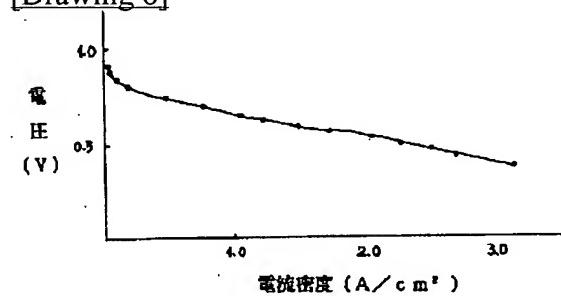
DRAWINGS

[Drawing 1][Drawing 2][Drawing 3][Drawing 4]

[Drawing 5]



[Drawing 6]



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